

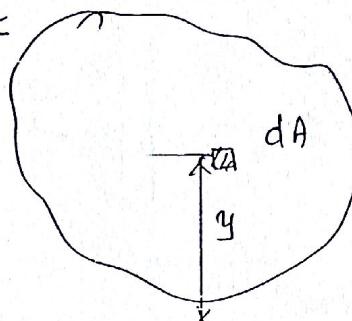
## UNIT - III

### MOMENT OF INERTIA:

#### Area Moment of Inertia:

In determining the strength of structural objects like beams, one comes across evaluation of mathematical expressions like  $\int y^2 dA$  where 'y' is the distance of an elemental area from a reference axis in the plane of the area. This is called the 'second moment' or 'Area Moment of Inertia'.

#### Definition of M.O.I. of an Area



If  $dA$  is an elemental area at a distance ' $y$ ' from the axis  $x-x$ ,

$\int y^2 dA$  is called the M.O.I. of  $A$  about  $x-x$ .

Obviously, the moment of inertia depends both upon the area and the axis. Therefore, while defining M.O.I., the axis must be specified.

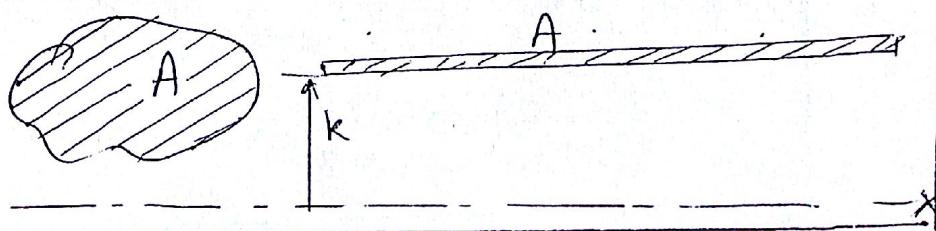
#### Radius of Gyration:

If  $I = \int y^2 dA = k^2 A$  where ' $A$ ' is the area, the number ' $k$ ' is called the radius of gyration and has units of length.

Units of M.I. are  $(\text{length})^4$  i.e.  $\text{mm}^4, \text{m}^4$  etc.

Significance of R.O.G.

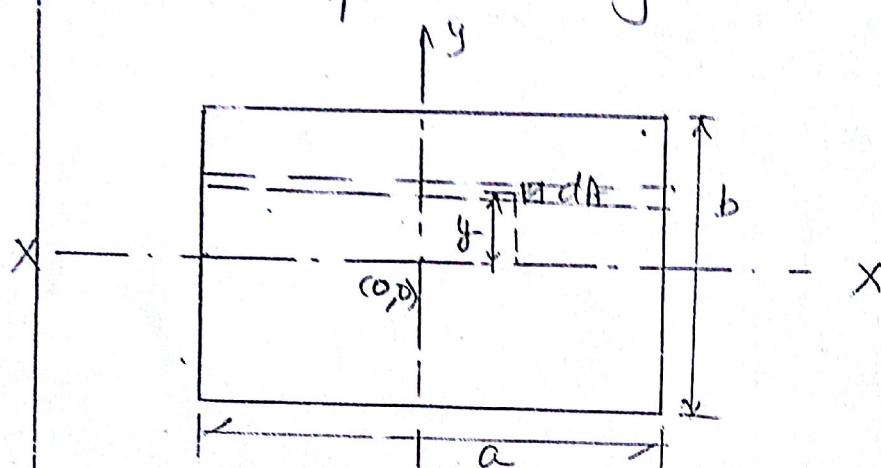
$$I = \int y^2 dA$$



If we imagine the given area 'A' of M.O.I. 'I', to be remoulded into a thin strip of area 'A' parallel to x-x axis such that its M.I. is equal to  $I_1$ , then the distance at which the strip must be placed so that this happens, is called the radius of gyration.

### Moment of Inertia of Simple Shapes:

#### I) M.I. of a rectangle



Let us consider a rectangular area  $dA = dx \cdot dy$  at a distance of  $y$  from x-x axis.

$$\text{M.I. of this element} = dA \cdot y^2 = dx \cdot dy \cdot y^2$$

If we now take a long strip of area of length ' $a$ ' and at a distance ' $y$ ' from x-x axis containing the element  $dx \cdot dy$ , the M.I. of this strip area

$$= \text{Area of the strip} \times y^2 \quad (\because y \text{ is same for all } dx \cdot dy \text{ elements})$$

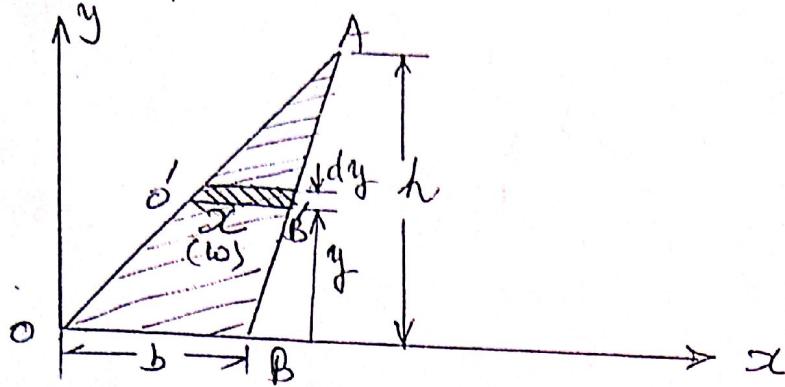
$$\text{i.e. } dI = \int_{b/2}^{a/2} y^2 dy \cdot dx = \int_{b/2}^{a/2} y^2 \cdot dA \quad (\text{where } dA = dx \cdot dy)$$

$$\therefore I_{xy} = \int_{-b/2}^{b/2} y^2 dA = \int_{-b/2}^{b/2} y^2 \cdot a \cdot dy = a \left[ \frac{y^3}{3} \right]_{-b/2}^{b/2}$$

$$\text{or, } I_{xx} = \frac{a}{3} \left[ \frac{b^3}{8} - \left( -\frac{b^3}{8} \right) \right] = \frac{1}{2} ab^3.$$

$$\text{Similarly, for a central } Y \text{ axis, } I_{yy} = \frac{1}{2} ba^3.$$

II) M.I. of triangle about its base:



Let the M.I. be required about an axis through the base  $X-X$  (coinciding with  $x$  axis for convenience).

Then, by definition,  $I_x = \int_A y^2 dA$ .

Let us consider an area strip parallel to the base ( $x$ -axis) at a distance of  $y$  and of length  $x'$  and height  $dy'$ .

$$\text{Then, } I = \int_A y^2 \cdot x \cdot dy$$

Now in  $\triangle OAB$  and  $\triangle O'AB'$ ,

$\triangle OAB$  is common, and  $O'B'$  &  $OB$  are parallel,  
Hence,  $\triangle OAB$  and  $\triangle O'AB'$  are similar,

$$\text{Therefore, } \frac{x}{b} = \frac{b-y}{h} \Rightarrow x = \frac{b}{h}(h-y)$$

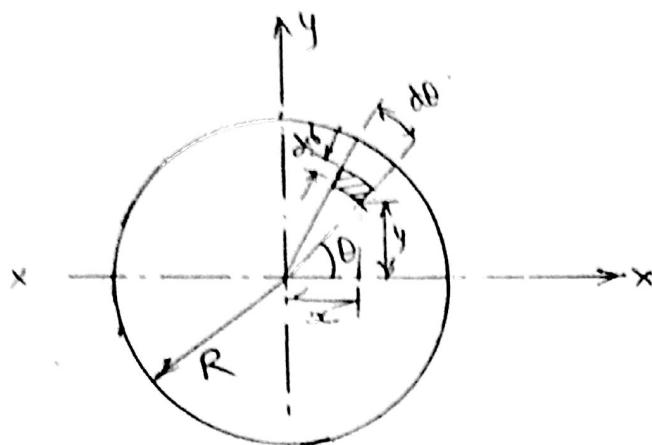
$$\therefore I = \int_A \frac{b}{h}(h-y) \cdot y^2 \cdot dy = \frac{b}{h} \int_0^h (hy^2 - y^3) dy$$

$$\text{or, } I = \frac{b}{h} \left[ \frac{hy^3}{3} - \frac{y^4}{4} \right]_0^h$$

$$= \frac{b}{h} \left[ \left( \frac{h^4}{3} - \frac{h^4}{4} \right) \right] = \frac{1}{12} bh^3$$

III) M.I. of a circular area about Diametral Ax.

Let us consider an area element  $r dr d\theta d\phi$  in polar coordinates. Then,  $I_{xx} = \int_0^{2\pi} \int_0^r r^2 \sin^2 \theta r dr d\theta d\phi$



$$x = r \cos \theta \\ y = r \sin \theta$$

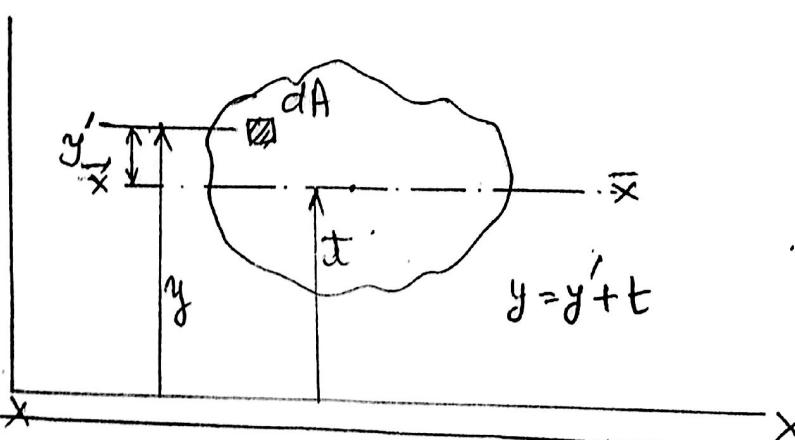
$$\begin{aligned} \therefore I &= \int_0^R \int_0^{2\pi} r^2 \sin^2 \theta \cdot dr \cdot d\theta = \int_0^R \int_0^{2\pi} (r^3 dr) \sin^2 \theta d\theta \\ &= \int_0^{2\pi} \left[ \frac{r^4}{4} \right]_0^R \sin^2 \theta d\theta = \frac{R^4}{4} \int_0^{2\pi} \sin^2 \theta d\theta \\ &= \frac{R^4}{4} \int_0^{2\pi} \left( 1 - \frac{\cos 2\theta}{2} \right) d\theta = \frac{R^4}{4} \left[ \frac{\theta}{2} - \frac{\sin 2\theta}{2} \right]_0^{2\pi} \\ \text{or, } I &= \frac{R^4}{4} \left[ \left( \frac{2\pi}{2} - 0 \right) - (0 - 0) \right] \\ &= \frac{\pi R^4}{4} \end{aligned}$$

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### Parallel and Perpendicular Axes theorems:

Parallel Axis (or Transfer Axis) Theorem.

The moment of inertia of an area A about <sup>parallel</sup> ~~an axis~~ to a centroidal axis in the same plane is equal to the M.I. of the same area about its centroidal axis + Area  $\times d^2$  where  $d$  is the distance between the centroid and the required axis.



Let us consider an element  $dA$  at a distance  $y$  from the required axis. Let  $d'$  be the distance between the reqd. axis and centroidal axis.

M.I. of the elemental area 'dA' about  $x$ - $x$

$$dI = y^2 \cdot dA = (y'+t)^2 \cdot dA$$

$$\text{or, } dI = (y'^2 + 2y't + t^2) \cdot dA.$$

Hence,  $I = \int_A (y'^2 + 2y't + t^2) dA$

$$= \int_A y'^2 dA + 2 \int_A y't dA + \int_A t^2 dA.$$

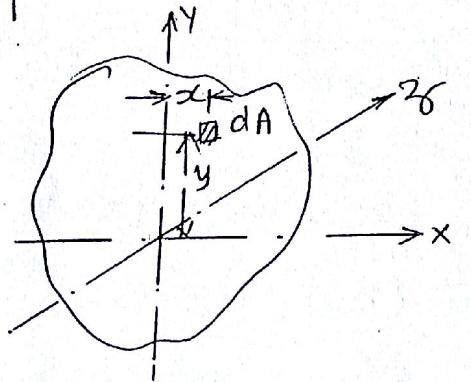
But, we know,  $2 \int_A y't dA = 2t \int_A y' dA = \bar{y} \cdot A$  where  $\bar{y}$  is the coordinate of C.G. of the area w.r.t.  $x'$  (which is zero)  $\Rightarrow \bar{y} \cdot A = 0$ .

and, since 't' is a constant,

$$\int_A t^2 dA = t^2 \int_A dA = t^2 \cdot A. \quad \dots \dots \dots (2)$$

Hence,  $I = \int_A y'^2 dA + t^2 A. \text{ or, } I = \bar{I}_x + A \cdot t^2$   
 $\underline{x} \quad \underline{x} \quad \underline{x} \quad \underline{x}$   
 $= \text{M.I. about parallel centroidal axis} + t^2 A.$

### Perpendicular Axis Theorem:



Let  $dA'$  be an area element in the  $x$ - $y$  plane as shown

Then

$$dI_x = y^2 dA, \text{ and}$$

$$dI_y = x^2 dA$$

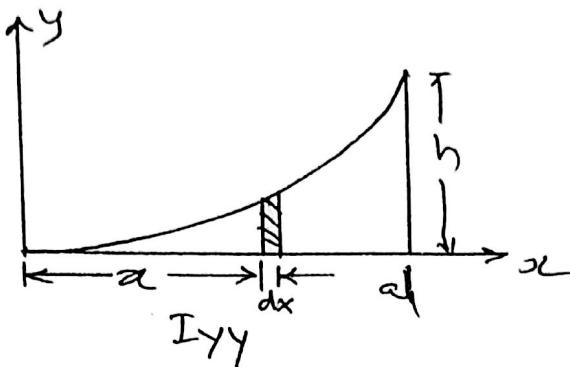
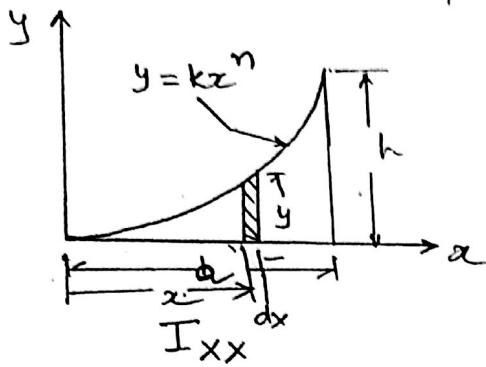
Hence,  $dI_x + dI_y = y^2 dA + x^2 dA$   
 $= (x^2 + y^2) dA.$

$$\text{Or but, } I_x + I_y = \int x^2 dA + \int y^2 dA$$

$$= \int_A (x^2 + y^2) dA = \int_A z^2 dA = I_z$$

Thus, the M.I. about 'z' axis passing thro. the intersection of  $x$  and  $y$  axes is the sum of M.I. about  $x$  &  $y$  axes.

To find out M.I. of a spandrel about coordinate axes. (24)



$$1) \underline{I_{xx}} : dI_{xx} = \frac{1}{3} y^3 dx = \frac{1}{3} (kx^n)^3 dx.$$

$$\therefore I_{xx} = \int_0^a \frac{1}{3} (kx^n)^3 dx = \frac{k^3}{3} \int_0^a x^{3n} dx$$

$$= \frac{k^3}{3} \left( \frac{x^{3n+1}}{3n+1} \right)_0^a = \frac{k^3 \cdot a^{3n+1}}{3(3n+1)}$$

$$\text{or, } I_{xx} = (k \cdot a^{3n+1}) \cdot a \times \frac{1}{3(3n+1)} = \frac{ah^3}{3(3n+1)} \dots$$

$$\text{Also, } \bar{I}_{xx} = I_{xx} - \frac{ah}{n+1} \cdot \left( \frac{n+1}{4n+2} \cdot h \right)^2$$

$$= \frac{ah^3}{3(3n+1)} - \frac{ah^3(n+1)}{(4n+2)^2} = \frac{ah^3}{3} \frac{(7n^2+4n+1)}{(3n+1)(4n+2)^2}$$

$$2) \underline{I_{yy}} : dI_{yy} = x^2 dA = x^2 y \cdot dx.$$

$$\text{or, } dI_{yy} = x^2 \cdot (kx^n) dx = kx^{n+2} dx$$

$$\rightarrow I_{yy} = k \cdot \int_0^a x^{n+2} dx = k \left[ \frac{x^{n+3}}{n+3} \right]_0^a$$

$$= \frac{ka^{n+3}}{n+3} = \frac{ah^3}{n+3} \dots$$

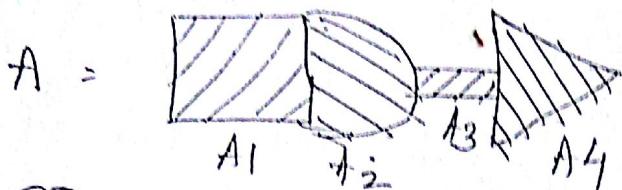
$$\text{Also, } \bar{I}_{yy} = \frac{ah^3}{(n+3)} - \frac{ah}{(n+1)} \cdot \left( \frac{n+1}{n+2} \cdot a \right)^2$$

$$= \frac{ah^3}{(n+2)^2 \cdot (n+3)} \dots$$

### MOMENT OF INERTIA OF COMPOSITE SECTIONS:

The moment of inertia of a composite section about a prescribed axis is found in the following steps.

- (I) The area is divided into geometrically simple shapes by adding (or subtracting) which the required area is formed.



- (II) The centroid of the areas is found using a convenient coordinate system if M.I. is required about centroidal axis.

- (III) For each of the part area, the M.I. is calculated about its own centroidal axis using appropriate formula.

- (IV) The M.I. of the areas for each area is transferred to the required axis using parallel axis theorem.

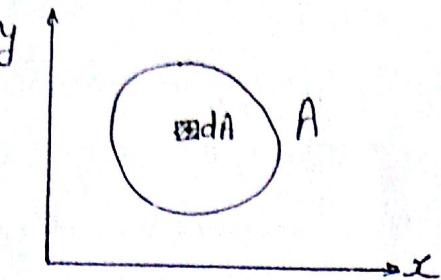
- (V) All the part M.I.'s about the required axis are added up to give the net M.I. about that axis.

- (VI) The whole operation is recorded in a Tabular format.

#### Important Points

i) M.I. of two areas can be added / subtracted only if it is about the same axis. Otherwise not.

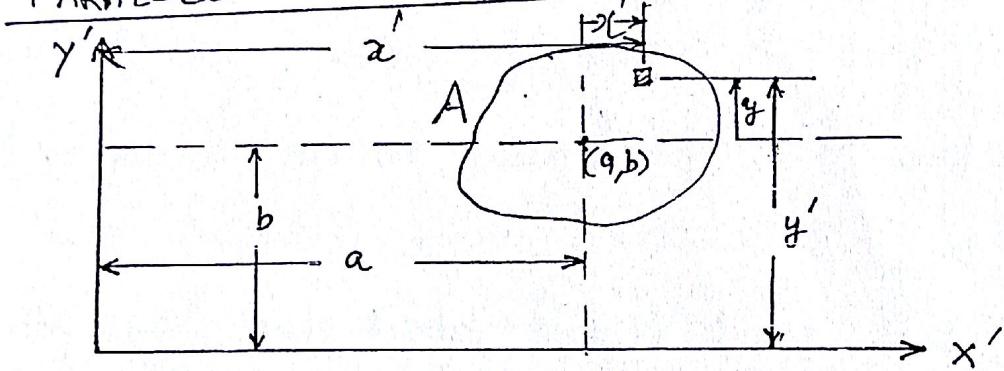
ii) Parallel axis theorem always requires identification of the centroidal axis of the concerned area.

PRODUCT OF INERTIA

$$I_{xy} = \sum x \cdot y \cdot dA = \int xy \, dA$$

The product of Inertia of an area w.r.t. to a coordinate axis system  $x-y$ , containing the area is defined as the sum  $\sum xy \, dA$  over the area  $A$ . In the limit as the sub areas  $dA$ 's in which  $A$  is divided tends to zero,  $\sum xy \, dA$  tends to the integral  $\int xy \, dA$  and is termed  $I_{xy}$ .

Unlike  $I_{xx}$  or  $I_{yy}$  which are always +ve,  $I_{xy}$  can be positive or negative.

PARALLEL AXIS THEOREM of P.O.I.

Let the P.O.I. of an area  $A$  w.r.t. to an axes system  $x'y'$  be  $P_{x'y'}$ :

$$P_{x'y'} = \int x'y' \, dA = \int x'y' \, dx' \, dy'$$

$$P_{x'y'} = \int (x+a)(y+b) \, dx \, dy, \quad \left\{ (a, b) \text{ being coordinates of CG of } A \right\}$$

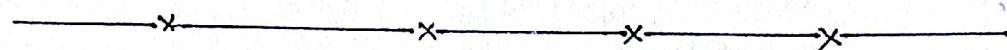
$$= \int (xy + xb + ay + ab) \, dx \, dy$$

$$= \int xy \, dA + b \int x \, dy + a \int y \, dx + ab \int 1 \, dA$$

But, by definition,  $\int x \, dA = 0$ ,  $\int y \, dA = 0$   
(when taken about centroidal axis).

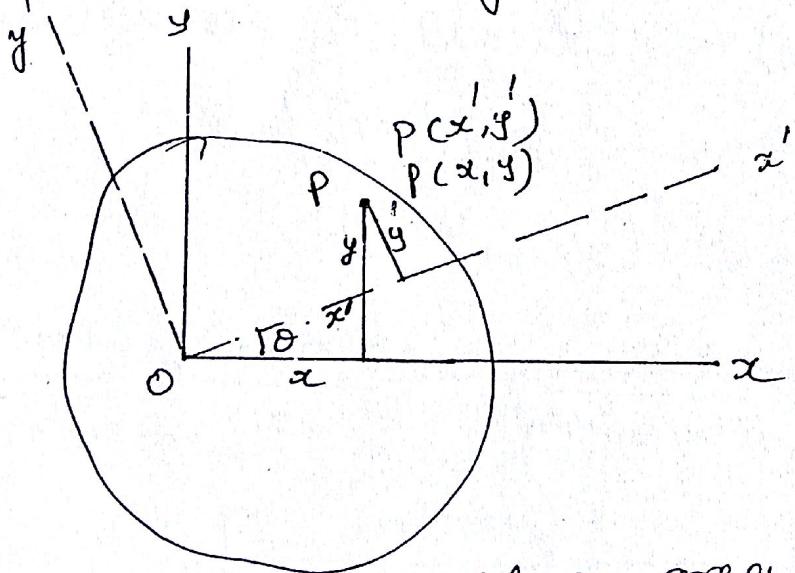
$$\therefore P_{x'y'} = \int xy \, dA + ab \cdot A \\ = I_{xy} + ab \cdot A.$$

Thus, the product of inertia about a set of axes is equal to the sum of product of inertia about a parallel set of axes through the C.G. of the area and the area times the product of coordinates of C.G.



### PRINCIPAL AXES OF INERTIA:

There exist two axes  $(x'$  and  $y')$  such that the P.I. about them is zero. These two perp. axes are ones about which M.I. is maximum and minimum. They are called the principal axes.



Let the P.I. of an area about an axis set  $xy$  be  $P_{xy}$ . Let  $x'y'$  be another set through the same origin at an angle  $\theta$  to  $x, y$ . Then,

$$x' = (x \cos \theta + y \sin \theta), \quad y' = (y \cos \theta - x \sin \theta).$$

$$\therefore P_{x'y'} = \int (x \cos \theta + y \sin \theta)(y \cos \theta - x \sin \theta) \, dx \, dy$$

$$\text{or, } P_{xy}' = \int \left\{ xy \cos^2 \theta - xy \sin^2 \theta + y^2 \sin \theta \cos \theta - x^2 \sin \theta \cos \theta \right\} dx dy$$

$$\text{or, } P_{xy}' = (\cos^2 \theta - \sin^2 \theta) \int xy dx dy + \left( \int (y^2 - x^2), dx dy \right) \times \frac{\sin 2\theta}{2}$$

$$= \cos 2\theta P_{xy} + \frac{\sin 2\theta}{2} (I_{xx} - I_{yy}) \quad \dots \dots \dots \textcircled{1}$$

$$\text{If } P_{xy}' = 0, \quad 2 \cos 2\theta \times P_{xy} = -\sin 2\theta (I_{xx} - I_{yy})$$

$$= \sin 2\theta (I_{yy} - I_{xx})$$

$$\therefore \tan 2\theta = \frac{2P_{xy}}{(I_{yy} - I_{xx})} \quad \dots \dots \dots \textcircled{2}$$

Since,  $P_{xy}$  and  $I_{yy}, I_{xx}$  are real & finite, there always exists an angle  $\theta$  such that  $\tan 2\theta$  is  $\left(\frac{2P_{xy}}{I_{yy} - I_{xx}}\right)$ . For this angle,  $P_{xy}' = 0$

Also, by differentiating  $P_{xy}'$  w.r.t.  $\theta$  and equating to zero,  $\frac{d}{d\theta}(P_{xy}') = -2 \sin 2\theta \cdot P_{xy} + \cos 2\theta (I_{xx} - I_{yy}) = 0$

$$\therefore \tan 2\theta' = \frac{(I_{xx} - I_{yy})}{2P_{xy}} \quad \dots \dots \dots \textcircled{3}$$

Substituting  $\textcircled{3}$  in  $\textcircled{1}$ , we get,

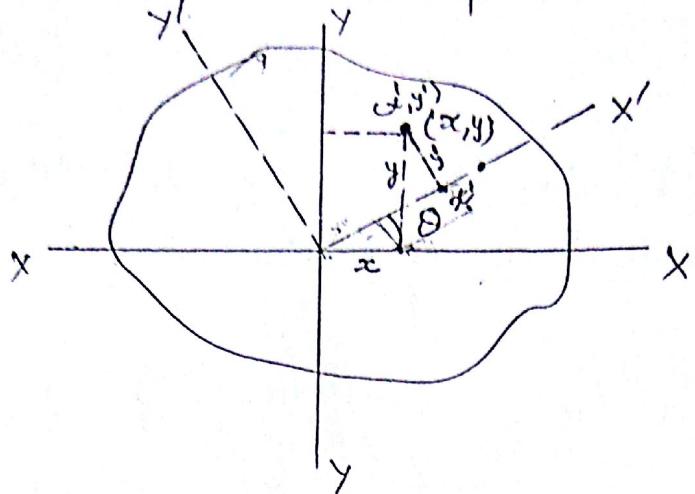
$$P_{xy\max}' = P_{xy} \cdot \frac{2P_{xy}}{\sqrt{(I_{xx} - I_{yy})^2 + 4P_{xy}^2}} + \frac{(I_{xx} - I_{yy}) \cdot (I_{xx} - I_{yy})}{2\sqrt{(I_{xx} - I_{yy})^2 + 4P_{xy}^2}}$$

$$= \frac{1}{2} \left[ \frac{4P_{xy}^2 + (I_{xx} - I_{yy})^2}{\sqrt{(I_{xx} - I_{yy})^2 + 4P_{xy}^2}} \right]$$

$$\therefore P_{xy\max}' = \frac{1}{2} \sqrt{(I_{xx} - I_{yy})^2 + 4P_{xy}^2} \quad \dots \dots \dots \textcircled{4}$$

$\textcircled{3}$  is the max. value of  $P_{xy}$  for two values of  $\theta'$  which are at rt. angles. For other two values of  $\theta$ ,  $P_{xy}' = 0$  and  $\theta$  and  $\theta'$  are at  $45^\circ$  to each other.

## Moment and Product of Inertia about Inclined Axes.



Let the coordinate axes be rotated through  $\theta$ . We know, from elementary transformations,

$$x' = x \cos \theta + y \sin \theta, \text{ and } y' = (y \cos \theta - x \sin \theta)$$

$$\text{Hence, } I_{x'x'} = \int (y \cos \theta - x \sin \theta)^2 dA$$

$$\begin{aligned} \text{or, } I_{x'x'} &= \int (y^2 \cos^2 \theta + x^2 \sin^2 \theta - 2xy \sin \theta \cos \theta) dA \\ &= \int \cos^2 \theta y^2 dA + \int x^2 \sin^2 \theta dA - \int xy \sin 2\theta dA \\ &= \cos^2 \theta \int y^2 dA + (\int x^2 dA) \sin^2 \theta - \sin 2\theta \int xy dA \\ &= \cos^2 \theta I_{yy} + \sin^2 \theta I_{xx} - \sin 2\theta P_{xy} \quad (1) \end{aligned}$$

(by definition).

Also, substituting  $x' = (x \cos \theta + y \sin \theta)$ , or alternatively, putting  $\theta = (\theta + 90^\circ)$

$$\begin{aligned} I_{y'y'} &= \cos^2(90 + \theta) I_{yy} + \sin^2(90 + \theta) I_{xx} - \sin 2(90 + \theta) P_{xy} \\ &= \sin^2 \theta I_{yy} + \cos^2 \theta I_{xx} + \sin 2\theta P_{xy} \quad (2) \end{aligned}$$

Adding (1) and (2), we get

$$I_{x'x'} + I_{y'y'} = I_{xx} + I_{yy} \quad (\text{first invariant})$$

$$\text{Also, } I_{x'x'} = \left( \frac{1+\cos 2\theta}{2} \right) I_{xx} + \left( \frac{1-\cos 2\theta}{2} \right) I_{yy} - \sin 2\theta P_{xy} \quad (30)$$

$$= \frac{(I_{yy}+I_{xx})}{2} + \frac{(I_{xx}-I_{yy})}{2} \cos 2\theta - P_{xy} \sin 2\theta. \quad (3)$$

For max.  $I_{x'x'}$ , differentiating (3) w.r.t  $\theta$ ,  
and equating to zero, we get

$$\leftarrow I_{x'x'}^{\max \min} = \left( \frac{I_{xx}+I_{yy}}{2} \right) \pm \sqrt{\left( \frac{I_{yy}-I_{xx}}{2} \right)^2 + P_{xy}^2} \quad (4)$$

$$\text{at } \theta = \frac{1}{2} \tan^{-1} \left( \frac{+2P_{xy}}{I_{yy}-I_{xx}} \right) \quad (5)$$

$$\text{Also, } P_{x'y'} = \int (x \cos \theta + y \sin \theta) (y \cos \theta - x \sin \theta) dA$$

$$= \int \{xy \cos^2 \theta - xy \sin^2 \theta + y^2 \sin \theta \cos \theta - x^2 \sin \theta \cos \theta\} dA$$

$$= \cos 2\theta \int xy dA - \frac{\sin 2\theta}{2} \left\{ \int x^2 dA - \int y^2 dA \right\}$$

$$= \cos 2\theta P_{xy} - \frac{(I_{yy}-I_{xx})}{2} \sin 2\theta.$$

$P_{x'y'}$  is 0 at a value of  $\theta$  given by

$$\tan 2\theta = \frac{2P_{xy}}{(I_{yy}-I_{xx})} \quad (6)$$

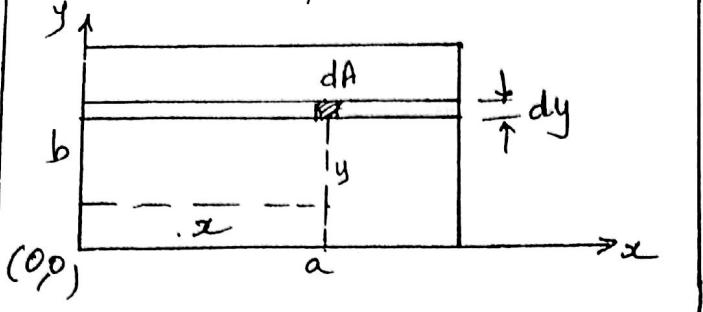
which is the value of  $\theta$  at which  $I$  is max./min.

$\therefore$  The two values of  $I_{x'x'}$  (Max. & min) are called 'Principal' values. All other values of  $I_{x'x'}$  lie between these two extreme values.

The principal values of  $P_{xy}$  are given by

$$P_{xy \max} = \pm \frac{1}{2} \sqrt{(I_{yy}-I_{xx})^2 + 4P_{xy}^2}$$

## Product of Inertia of a Rectangle:-

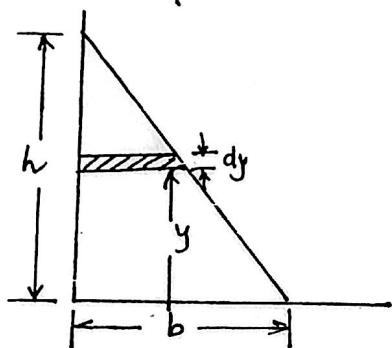


For the infinitesimal strip parallel to x axis between y and  $y+dy$

$$dP = \int xy \, dA = \int y \cdot dy \int x \, dx \\ = \left[ \frac{y^2}{2} \cdot \left( \frac{a^2}{2} \right) \right]$$

$$\text{or, } P = \frac{a^2}{2} \int_0^b y \, dy = \frac{a^2}{2} \cdot \frac{b^2}{2} = \frac{a^2 b^2}{4} - \textcircled{1}$$

P.I. of a triangular area (right angled)



For a strip parallel to x axis at y

$$dP = \int xy \, dA = y \int x \, dx \\ = y \cdot \left[ \frac{x^2}{2} \right] = \frac{x^2}{2} y \, dy$$

$$\text{But, } \frac{x}{b} = \frac{h-y}{h}, \rightarrow x = \frac{b}{h}(h-y)$$

$$\therefore dP = \frac{b^2}{2h^2} (h-y)^2 \cdot y \, dy = \frac{b^2}{2h^2} \{ h^2 y - 2hy^2 + y^3 \} \, dy$$

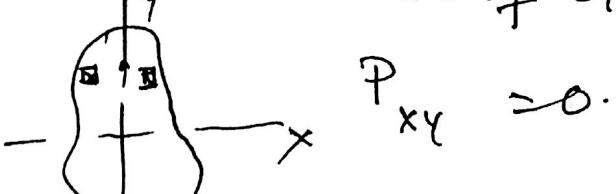
$$\therefore P = \frac{b^2}{2h^2} \int_0^h \{ h^2 y - 2hy^2 + y^3 \} \, dy = \frac{b^2}{2h^2} \left[ \frac{h^2 y^2}{2} - \frac{2hy^3}{3} + \frac{y^4}{4} \right]_0^h$$

$$\text{or, } P = \frac{b^2}{2h^2} \left[ \frac{h^4}{2} - \frac{2h^4}{3} + \frac{h^4}{4} \right] = \frac{b^2 h^2}{24}$$

$$\overline{P}_{(\text{c.g.})} = \frac{b^2 h^2}{24} - \left( \frac{b}{3} \cdot \frac{b}{3} \right) \cdot \frac{b \cdot h}{2} = b^2 h^2 \left\{ \frac{1}{24} - \frac{1}{18} \right\} - \textcircled{2}$$

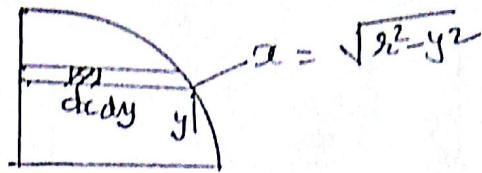
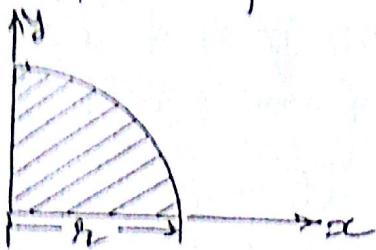
$$= - \frac{1}{72} (b^2 h^2) - \dots - \textcircled{3}$$

I about an axis of symmetry is zero.



(32)

Find the Product of Inertia of a quarter of a circular area in the first quadrant about its edges.



$$dI = x \cdot y \cdot dx \cdot dy$$

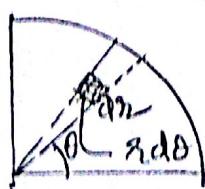
For a strip of constant  $y$ ,  $dI_{\text{strip}} = \int_0^x xy \, dx \, dy$

$$dP_{\text{strip}} = (y \, dy) \int_0^x x \, dx = \left(\frac{x^2}{2}\right) y \, dy$$

$$P_{\text{strip}} = \int_0^r \frac{x^2}{2} y \, dy = \int_0^r \left(\frac{r^2 - y^2}{2}\right) y \, dy$$

$$\text{or, } P = \frac{1}{2} \int_0^r (r^2 y - y^3) \, dy = \frac{1}{2} \left[ \frac{r^2 y^2}{2} - \frac{y^4}{4} \right]_0^r \\ = \underline{\underline{\frac{1}{8} r^4}}$$

Alternatively,  $dP = d(r) (r \, d\theta) x \cdot y$



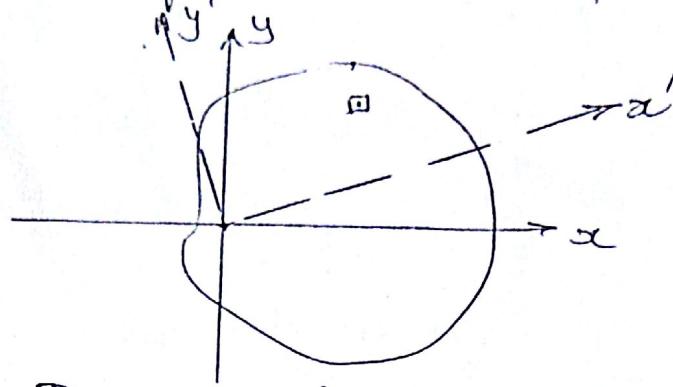
$$= r \, dr \, d\theta \cdot r \cos \theta r \sin \theta$$

$$P = \int_0^{\pi/2} \int_0^r r^2 \cdot dr \cdot \sin \frac{2\theta}{2} d\theta$$

$$= \frac{1}{2} \left[ \frac{r^4}{4} \right]_0^r \left[ \frac{\cos 2\theta}{2} \right]_0^{\pi/2} = \frac{1}{2} \cdot \frac{r^4}{4} \cdot \frac{1}{2} [(-1) - (1)] \\ = \underline{\underline{\frac{r^4}{8}}}$$

Reciprocal moment of inertia.

(33)



$$x' = x \cos \theta + y \sin \theta$$

$$y' = y \cos \theta - x \sin \theta$$

$$\begin{aligned} P_{x'y'} &= \int (x \cos \theta + y \sin \theta)(y \cos \theta - x \sin \theta) dA \\ &= \int xy (\cos^2 \theta - \sin^2 \theta) dA + \int \cos^2 \theta y^2 dA - \int x^2 \cos^2 \theta dA \\ &= \cos 2\theta \int xy dA + \left[ \frac{y^2}{2} \right] - \left[ \frac{x^2}{2} \right] = 0 \\ \text{or, } P_{xy} \cos 2\theta + (I_{xx} - I_{yy}) \frac{\sin 2\theta}{2} &= 0 \end{aligned}$$

When  $P_{x'y'} \text{ is zero}$   
 $\tan 2\theta = (2P_{xy} / (I_{yy} - I_{xx}))$

$$\theta = \frac{1}{2} + \tan^{-1} \left( \frac{2P_{xy}}{I_{yy} - I_{xx}} \right) \quad \text{--- (1)}$$

Also,

$$\begin{aligned} I_{x'x'} &= \int (x \cos \theta + y \sin \theta)^2 dA \\ &= \int (x^2 \cos^2 \theta + y^2 \sin^2 \theta + 2xy \cos \theta \sin \theta) dA \\ &= \cos^2 \theta \int x^2 dA + \sin^2 \theta \int y^2 dA + \sin 2\theta \int xy dA \end{aligned}$$

or,  $I_{x'x'} = \cos^2 \theta I_{yy} + \sin^2 \theta I_{xx} + \sin 2\theta P_{xy}$

But,  $\cos^2 \theta = \frac{1 + \cos 2\theta}{2}$ , &  $\sin^2 \theta = \frac{1 - \cos 2\theta}{2}$

$$\therefore I_{x'x'} = \frac{1}{2} (I_{xx} + I_{yy}) + \frac{(I_{xx} - I_{yy}) \cos 2\theta}{2} + \sin 2\theta P_{xy}$$

and,

$$\begin{aligned} I_{y'y'} &= \frac{1}{2} (I_{xx} + I_{yy}) - \frac{(I_{xx} - I_{yy}) \cos 2\theta}{2} - \sin 2\theta P_{xy} \quad \text{--- (2)} \end{aligned}$$

Hence,  $I_{x'x'} + I_{y'y'} = I_{xx} + I_{yy}$

(1<sup>st</sup> invariant of M.O.I.) - (2)

For Max  $I_{x'x'}$ ,  $dI_{x'x'}/d\theta = 0$

$$\therefore \left( \frac{I_{xx} - I_{yy}}{2} \right) (-2 \sin 2\theta) + 2 \cos 2\theta P_{xy} = 0$$

$$\text{or}, \quad (I_{yy} - I_{xx}) \frac{\sin 2\theta}{2} = 2 P_{xy} \cos 2\theta$$

$$\text{or}, \quad \tan 2\theta = \frac{2P_{xy}}{(I_{yy} - I_{xx})}$$

$$\text{i.e. } \theta = \frac{1}{2} \tan^{-1} \left( \frac{2P_{xy}}{I_{yy} - I_{xx}} \right)$$

which is the same value of  $\theta$  for which  $P_{x'y'}^2 = 0$

∴ Principal axes are those for which the product of inertia is zero and M.I. is either a maximum or minimum.

PROBLEMS

CENTRE OF GRAVITY / CENTROID: (\*)

6-5. 5, 6, 7, 8, 9

6-6. 4, 5, 8, 9, 13, 14, 15, 16, 18, 19, 20, 21

6-7. 3, 4, 5, 6, 8, 9, 10, 13.

6-8. 3, 4, 5, 6, 9, 11

MOMENT OF INERTIA / PRODUCT OF INERTIA

7-5. 4, 5, 6, 7, 8, 10, 12

7-6. 7, 8, 9, 10, 12, 14

7-9. 2, 6, 11, 12

7-12. 5, 6.

(\*) Singers' Engineering Mechanics  
Statics and Dynamics,  
K.V.K. Reddy, J. Suresh Kumar.